

The Astrophysical Plasmadynamic Explorer (*APEX*): A High Resolution Spectroscopic Observatory

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The Astrophysical Plasmadynamic Explorer (APEX): A High Resolution Spectroscopic Observatory

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ABSTRACT

EUVE and the *ROSAT WFC* have left a tremendous legacy in astrophysics at EUV wavelengths. More recently, *Chandra* and *XMM-Newton* have demonstrated at X-ray wavelengths the power of high-resolution astronomical spectroscopy, which allows the identification of weak emission lines, the measurement of Doppler shifts and line profiles, and the detection of narrow absorption features. This leads to a complete understanding of the density, temperature, abundance, magnetic, and dynamic structure of astrophysical plasmas. However, the termination of the *EUVE* mission has left a gaping hole in spectral coverage at crucial EUV wavelengths ($\sim 100\text{-}300$ Å), where hot ($10^5\text{-}10^8$ K) plasmas radiate most strongly and produce critical spectral diagnostics. *CHIPS* will fill this hole only partially as it is optimized for diffuse emission and has only moderate resolution ($R\sim 150$). For discrete sources, we have successfully flown a follow-on instrument to the *EUVE* spectrometer ($A_{\text{eff}}\sim 1$ cm², $R\sim 400$), the high-resolution spectrometer *J-PEX* ($A_{\text{eff}}\sim 3$ cm², $R\sim 3000$). Here we build on the *J-PEX* prototype and present a strawman design for an orbiting spectroscopic observatory, APEX, a SMEX-class instrument containing a suite of 8 spectrometers that together achieve both high effective area ($A_{\text{eff}}\sim 20$ cm²) and high spectral resolution ($R\sim 10,000$) over the range 100-300 Å. We also discuss alternate configurations for shorter and longer wavelengths.

Keywords: Satellite Instruments, Spectrometers, Diffraction gratings, Multilayer coatings, Extreme Ultraviolet

1. INTRODUCTION

Spectroscopy has evolved into an indispensable tool in the task of measuring the composition, density, temperature, velocity and magnetic field of astrophysical plasmas. Now *EUVE*, *Chandra* and *XMM-Newton* have moved astronomical spectroscopy into the EUV and X-ray wavebands, where hot ($10^5\text{-}10^8$ K) plasmas radiate most strongly. However, further developments are needed to exploit the full range of plasma diagnostic techniques developed in laboratory and solar physics, including instruments of higher resolution, in particular spectrometers which could, for example, resolve and measure spectral lines unambiguously and measure line profiles and Doppler shifts. A desirable goal is a resolving power $R>10,000$ ($\lambda=0.01$ Å at 100 Å, or $V=30$ km s⁻¹). The EUV waveband between 100 and 300 Å is most promising for high-resolution spectroscopy of hot plasmas, for the following reasons:

- (1) The interstellar medium (ISM) has relatively low opacity out to distances of order 100 pc and is patchy, allowing diverse galactic studies and some extragalactic observations.
- (2) There are many strong spectral lines produced by plasmas at temperatures between 2×10^5 and 2×10^7 K.¹
- (3) Multilayer-coated, normal-incidence optics may be used. They have smaller aberrations than grazing-incidence optics, promise large collecting area, and allow designs with a single optical element.

In this paper we present a strawman design for an orbiting high-resolution EUV spectroscopic observatory, APEX, the Astrophysical Plasmadynamic EXplorer, a SMEX (SMall EXplorer) class instrument.

2. SCIENCE JUSTIFICATION

It is difficult to predict the course of EUV astronomy following the *EUVE* and *ROSAT* Wide Field Camera (*WFC*) missions, but in regard to high-resolution spectroscopy we give as examples four research areas with exciting prospects. The first is the formation and characteristics of hot coronae around pre-main-sequence (PMS) stars, stars on the main sequence (MS), subgiants and the hotter giant stars. The driving force is the magnetic dynamo in stellar convection zones, which is most active and volatile when a star is young and in the PMS stage. There are violent eruptions of field from the star, which may play an important role as planetary systems start to evolve. The activity diminishes after the star enters the MS, but our sun shows how complex this activity is and how it influences conditions around the planets. Thus at some point searches for life in other planetary systems must take into account the influence of the stellar corona. When the sun is compared to more active stars, where the energy released may be up to 10^4 times that in solar events, the difficulties of understanding stellar dynamos as a galactic phenomenon become apparent. The study of stellar dynamos is bound to the study of the distribution, temperature, density, composition and dynamics of the hot coronal plasma, and of the origin of active regions, loops and flares. Solar research has demonstrated the importance of high-resolution spectroscopy in such research.

The second area is to understand how stars evolve from the giant branch into the white dwarf (WD) region of the H-R diagram. The formation and evolution of WD stars is a major facet of galactic evolution, and their distribution and characteristics are important in estimating the age and mass of the galaxy. The third area is the study of accretion in cataclysmic variable (CV) systems. For example, the large width of some AM Her spectral lines implies that turbulence or Zeeman splitting is at work in the accretion flow, and to clarify the accretion disk behavior during dwarf novae outbursts the time-dependence of selected lines needs to be established. Both tasks require high-resolution spectroscopy. The fourth area is the study of He in the local interstellar medium (LISM) by making high-resolution measurements of HeII absorption lines in WD spectra. Helium is the element most sensitive to non-equilibrium ionization conditions, and is a sensitive indicator of ionizing sources in the LISM. HeII and HeI measurements could test whether the gas in the LISM is in an ionization recombination phase following a supernova a few million years ago. This would be an important adjunct to the CHIPS mission to survey the structure, ionization state and cooling processes of the 10^6 K gas in the LISM. The table below shows the wide variety of targets relating to these areas that would be covered by *APEX*.

Table 1. Extracts from an Extensive APEX Target List

Target	White Dwarf	Cool Star	CV	Extragalactic	Comments
GD659	x				Pure H, He II, ISM Detection with EUVE, prime ISM target
FEIGE 245	x				DA+dm binary, DA has metals; ISM and evolution studies
G191-B2B	x				DA+metals, best studied very hot DA for diffusion/levitation
GD 71	x				Pure H, low nH, prime ISM target
SIRIUS B	x				Nearest WD, massive and important for evolution and ISM
PG 1123+18	x				Hot DA+metals, He II, important for levitation/diffusion and ISM
EG 187	x				Intermediate temp DA, low nH, prime ISM target
HZ 43	x				Archetypal hot DA, low nH, prime ISM target and cal source
REJ2156-843	x				Pure H DA, He II detection with EUVE; prime ISM target
REJ2214-491	x				? Hottest DA+metals, extreme case for levitation/diffusion
V471 Tau	x	x			Pre-CV; K2V+DA, $p=0.62d$
VV Pup			x		Magnetic CV, very soft X-ray flux, funneled flow, $p_{orb}=p_{gap}=0.06975d$
U Gem			x		Non-magnetic CV (dwarf nova) with X-ray outbursts, $p=0.177d$
SS Cyg			x		Normal/super outburating non-magnetic white dwarf in CV, $p=0.275d$
Procyon		x			Thin convection zone; solar-like activity
α Cen AB		x			Solar-like activity; K star dominates ~2:1
Prox Cen		x			EUV - brightest "low" activity late M dwarf
AU Mic		x			Very active M dwarf
β Cet		x			First sec. or clump giant
AB Dor		x			Pre-MS, $p=0.51d$
α Aur		x			RS CVn Asynchronous binary; Hertzsprung gap + clump?
AR Lac		x			RS CVn $p=2.0d$, $i=57$ degrees, eclipsing
VS Cep		x			W Uma contact binary: $p=0.28d$
YY Gem		x			By Draconis-like flare star, eclipsing, $p=0.8d$, $i=86$ degrees
PKS 2155-304				x	BL Lacertae object ($z=0.17$)

These four areas are also part of the NASA major theme “*Structure and Evolution of the Universe*”, and pursue Objective 3 of the NASA Strategic Plan for Space Science. However the first area has a broader context and is linked to the other major themes, “*The Sun-Earth Connection*” and “*Astronomical Search for Origins*”, and to Objectives 7 (“*Understand our changing Sun and its effects throughout the Solar System*”) and 4 (“*Look for signs of life in other planetary systems*”) of the NASA Strategic Plan.

Fig. 1 compares the observed spectrum (black error bars) with model predictions (red histogram) based on a homogeneous composition stellar atmosphere and including interstellar HI, HeI and HeII absorption. The HI and HeI column densities were fixed at values obtained from analysis of the broader band, lower resolution EUVE spectrum, and the values of T and g were taken from the latest optical analysis (T=54,000K, log g=7.5).^{6,7} The interstellar HeII column density and photospheric He abundance were allowed to vary freely, and the best match to the model was obtained by minimizing a Cash statistic. The best-fit model folded through the *J-PEX* instrument response assumed a resolving power of 4000 (0.057 μ FWHM), and the data's S/N averaged 5.0 per sampling bin. The observed spectrum shows a continuum modulated by numerous absorption lines and by absorption in the ISM. The good agreement between the model and the data is striking, with the most prominent resolved feature a strong OIV absorption line at 233.5 \AA . Between \sim 227 and 232 μ is a broad "bump", a characteristic of the overlapping series of interstellar HeII absorption lines superposed on a continuum. Taken together with the strong depression of the flux below 227 μ , this is conclusive proof that interstellar or circumstellar HeII is present in the line of sight. The strongest expected photospheric line at 243 \AA was too close to the noise level to claim a direct detection of photospheric helium as yet. However, the best fit was obtained for $N_{\text{HeII}}=5.97 \times 10^{17} \text{cm}^{-2}$ and $\text{He/H}=1.6 \times 10^{-5}$, and the joint confidence contour for these parameters produced 99% confidence limits of $(5.76\text{-}6.18) \times 10^{17} \text{cm}^{-2}$ for N_{HeII} and $(1.31\text{-}1.91) \times 10^{-5}$ for He/H .

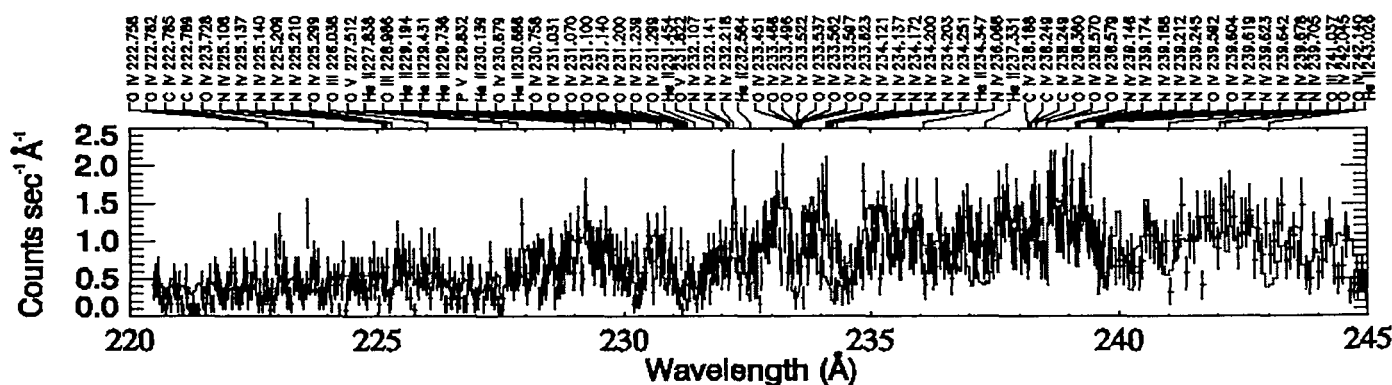


Fig. 1. High-resolution spectrum of G191-B2B obtained by the *J-PEX* spectrometer in the band 220-245 Å (error bars). The red histogram is the best-fit model of the stellar photosphere and the ISM (see text). The strongest predicted lines of He, C, N, O, and P are labeled by ionization state and wavelength. Fe and Ni lines, too numerous to list, produce the unlabelled features and the broader absorption structures.

3. APEX STRAWMAN DESIGN

The *J-PEX* sounding rocket payload had two advantages, high A_{eff} and R , and two disadvantages, a limited bandwidth and limited observation time. Specific scientific questions can be addressed effectively using sounding rockets, but studying the large and diverse samples revealed by *EUVE* and the *ROSAT WFC* requires the long observation times provided by an orbiting observatory. Moreover, a *SMEX* satellite affords much more volume than a sounding rocket so that the bandwidth problem may be overcome by using several spectrometers, each optimized for a different waveband. *APEX* fits comfortably within the Taurus 2210 payload shroud of a *SMEX* (Fig. 2) and contains no moving parts (other than the payload door) hence minimizing risk.

Fig. 3 shows the instrument aperture. *APEX* contains a suite of 8 spectrometers, each having a grating, a collimator, and a detector. Each spectrometer is mounted on an optical bench, which is isolated from thermal and vibrational loads in the payload structure. The optical bench also provides independent capability to align and focus the gratings during calibration and flight. The aperture end of the payload contains the collimators, the detectors, instrument support electronics (not shown), the payload door (not shown), and the star tracker used in acquiring targets (not shown). The opposite end contains the gratings and other payload support system (payload command and control electronics, batteries, ACS, telemetry, etc.). Unfolding solar cell panels would reside before launch in the annular volume between the *APEX* outer skin and the maximum payload envelope. The honeycomb collimator modules restrict the field of view ($\sim 1^\circ$) to limit the diffuse EUV and UV radiation that enters the spectrometers, and *J-PEX* has provided us with much experience in designing and fabricating suitable modules.⁹ This radiation is further attenuated to acceptable levels using a thin-film filter mounted inside each detector vacuum enclosure slightly upstream of its photocathode. (Thus the filter suffers no acoustic loads during T&E and launch.) *J-PEX* used an aluminum filter mounted on a nickel mesh, and suitable materials are available for all the wavebands discussed in this paper. Internal baffles (not shown) trap and attenuate unwanted diffracted orders, zero order, and scattered light from the gratings. Because sounding rocket observation times are short, *J-PEX* was launched under vacuum to ensure adequate time for outgassing. No such requirement exists for a satellite instrument; however, it may be desirable to make the payload door a vacuum seal (or doors for each spectrometer) for ease in handling during calibration. During idle periods the payload would be backfilled with an inert gas to retard contamination and degradation of the multilayer-coated optics.

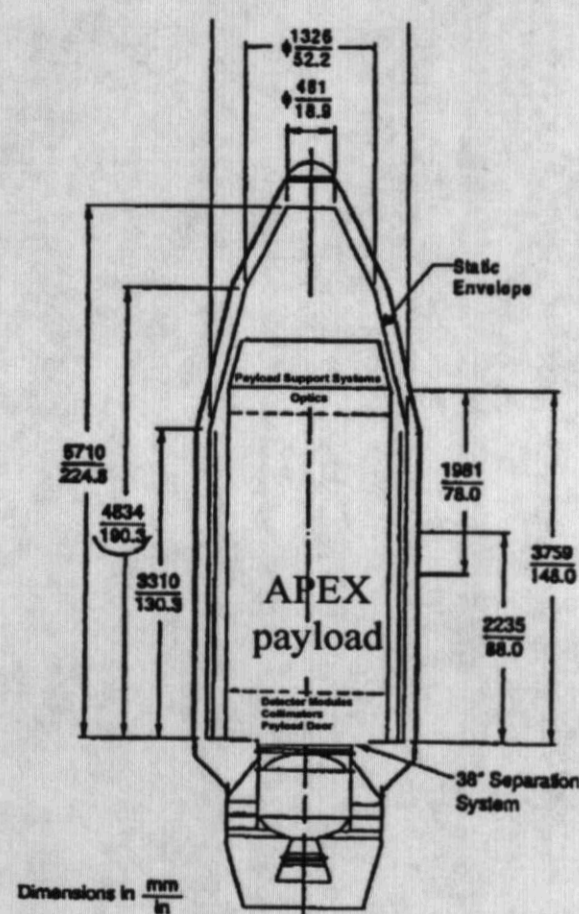


Fig. 2. *APEX* payload in Taurus 2210 shroud.

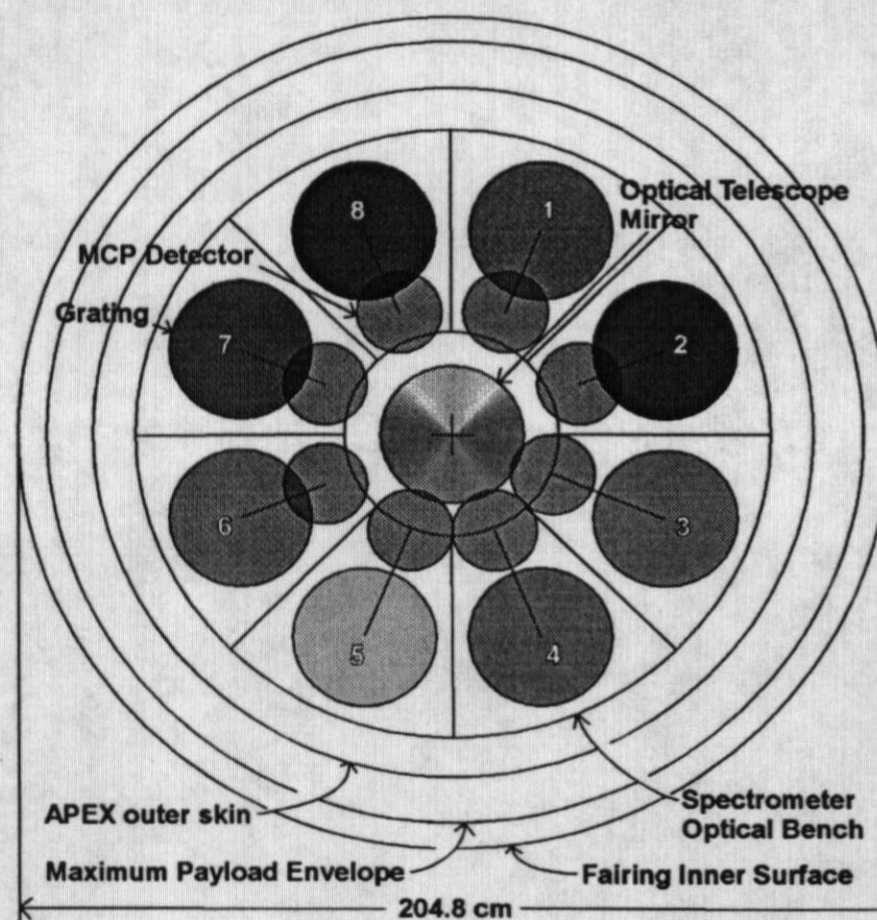


Fig. 3. *APEX* Instrument Aperture.

Each microchannel plate (MCP) detector would have its own vacuum enclosure to allow operation independent of the spectrometer. For simplicity a circle of diameter 200 mm was chosen as the detector footprint for this strawman payload. However, the size and shape of these enclosures is under study, and therefore the slight obscuration of the grating by the detector in some of the spectrometers (Fig. 3) should not be taken seriously. Each detector would have multiple MCPs (e.g., chevron or Z-stack configuration) to produce high gain in saturation mode with low background noise. Both high quantum

efficiency (QE) and high spatial resolution, especially in the dispersion direction (the line shown in projection that connects the grating and detector centers), are essential for sensitive high-resolution spectroscopy. At EUV wavelengths, QE is dominated by the photoelectric yield of the top MCP and its photocathode. Common choices of photocathodes include CsI and KBr. Spatial resolution is determined by the pore spacing of the MCPs and by the charge collection anode. Glass MCPs produced from boules using heating and drawing techniques have been the standard for many years, and channel diameters of 12.5 μm and more recently 6 μm are available. *J-PEX* used a chevron configuration of glass MCPs with a CsI photocathode deposited on the top MCP. However, current research with silicon MCPs has produced results that promise to surpass the performance of glass MCPs without encountering any of their problems, and these may be considered for use in *APEX*.¹⁰ A number of anodes are available that produce high-resolution images including the vernier anode,¹¹ delay-line anodes,¹⁰ and cross-strip anodes.¹⁰ The *J-PEX* MCP detector used a vernier anode that produced high linearity with a resolution less than 20 μm , which is adequate for *APEX*. However, further development with all these anodes has been very successful, leading to images of 6 μm MCP pores.

The figured gratings are all mounted in a Wadsworth configuration operating at near-normal incidence. They have a focal length of 3 m and a diameter of 340 mm. With allowance for the footprint and volume of support subsystems no more than 8 such gratings can fit within a payload designed for the Taurus 2201 shroud. Grating details are given in the following sections. As with *J-PEX*, the *APEX* payload also contains a telescope operating at optical/UV wavelengths. The telescope mirror is 340 mm in diameter, and a CCD camera (not shown) is mounted at its prime focus. This telescope is co-aligned to the spectrometers and views the target and/or adjacent stars. Its purpose is to provide an accurate aspect measurement while on target. Each spectral photon is time-tagged and interpolation between CCD images produces an accurate measurement of the instantaneous pointing direction when the photon was recorded. Thus *APEX* does not require high pointing accuracy, only that payload jitter rates be small enough so that the CCD images can be interpolated accurately. This type of telescope proved highly successful on the *J-PEX* mission, and the larger *APEX* mirror provides more sensitive measurements (the *J-PEX* mirror was only 135 mm in diameter).

4. EFFECTIVE AREA FOR *APEX* BASELINE CONFIGURATION

The EUV flux from all astrophysical objects other than the sun is relatively weak. Although observation times in a satellite may be as large as needed, many of the *APEX* targets vary on dynamical time-scales of hours to days. Thus high A_{eff} is necessary to produce temporally resolved high-resolution spectra. The simple *APEX* optical design means that the effective area of each spectrometer is the product of only 5 factors: the transmittance of the collimator, the geometrical area of the grating, the efficiency of the grating, the transmittance of the filter, and the QE of the MCP detector. It is beyond the scope of this paper to investigate all these factors in detail, but the goal is to maximize all them. Little can be done to improve collimator transmittance, which is already 85-90%. Thinner filters have higher transmittance, but are more difficult to fabricate without pinholes, are more fragile, and transmit more unwanted diffuse EUV/UV radiation. Therefore, filter thickness and ultimately transmission is a tradeoff among these competing requirements. In the following calculations of effective area, filter transmittances were derived using on-line software available at the Center for X-ray Optics website (<http://www-cxro.lbl.gov/>). We assumed all filters were mounted on a mesh with 85% transmittance. MCP detector QE values were taken from the literature and at EUV wavelengths are in the range 15-60%. Collimator transmittance was assumed to be 90%. In the remainder of this paper we concentrate on grating issues (area and efficiency).

For over a decade we have pursued the goal of achieving high efficiency in a normal-incidence instrument by using ultra-smooth holographic ion-etched gratings that have been coated with high-reflectance multilayers.¹² We have measured efficiencies in the range 5-16% with both laminar and blazed gratings at wavelengths between 100 and 300 Å,¹³⁻¹⁷ and in the laminar case the groove efficiency of the underlying grating substrate now approaches the theoretical limit for the first order of 40.5%.¹⁸ For the scalar regime in which we operate, the measured grating efficiency is the product of the grating groove efficiency and the reflectance of the coating (whether a multilayer, single layer, or bare surface), and so there are essentially 6 factors in calculating effective area. Moreover, our investigations have produced excellent agreement between theoretical models and measurements for multilayers,¹³⁻¹⁷ bare ion-etched gratings,^{19,20} and multilayer gratings.¹³⁻¹⁷ Finally, we have shown that the dispersive characteristics of gratings are unchanged with the application of the multilayer, and in one case a diffraction-limited resolving power of 14,000 was achieved.²¹

All these research results were obtained using relatively small (~25 mm diameter) sample gratings. However, *J-PEX* contained four large (160x90 mm) identical spherical laminar gratings, coated with identical multilayers, and mounted in a off-axis Wadsworth configuration. Progress has been steady at a number of commercial vendors (e.g., Zeiss, Jobin-Yvon) in the fabrication of large area gratings. High-quality ion-etched gratings of diameter 340 mm are now feasible and we have

baselined them for *APEX*. Systems for the deposition of high-reflectance multilayers uniformly over large areas have been available for several years now at the Lawrence Livermore National Laboratory (e.g., *J-PEX*, *TRACE*) and elsewhere. Multilayer technology is also backed by accurate theoretical models and a vast database of measured material properties.

As part of the *J-PEX* calibration effort we mapped the efficiency of the gratings after multilayer coating at the Naval Research Laboratory beamline X-24C at the National Synchrotron Light Source, Brookhaven National Laboratory.^{22,23} This facility consists of a grating-crystal monochromator,^{24,25} to disperse the synchrotron light, and a number of selectable thin-film filters, which suppress high-order radiation from the monochromator and provide absorption edges for wavelength calibration. The *J-PEX* gratings were calibrated in a reflectometer,²⁶ and a recent upgrade to this facility allows for the calibration of *APEX*-sized gratings. For *J-PEX*, the average measured peak efficiency (@ 234 Å) ranged from 10.3±0.6% for the best grating to 7.2±1.2% for the worst. (Problems with cleaning procedures, since remedied, reduced the efficiency of two gratings.) The quoted uncertainty is dominated by the standard deviation in the number of measurements (~20), and may be taken as a measure of uniformity, which was less than 10% for the best gratings. The instrumental uncertainties are small in both the measured efficiency (1-3% of the measured value) and the wavelength scale (0.3 Å),²⁷ giving us strong confidence that *APEX* could be calibrated accurately.

The most efficient *J-PEX* gratings had groove efficiencies in the range 31-34%, approaching the theoretical limit of 40.5% for a laminar grating used in the first inside order. However, blazed gratings offer two distinct advantages over laminar gratings. First, the groove efficiency of an ideal blazed grating can approach 100%. Second, this performance may be achieved in higher grating orders, allowing the groove density to be held within practical bounds at the shorter wavelengths or in applications demanding higher resolving power. However, to date difficulties in manufacturing an ideal blazed groove profile of low roughness at the low blaze angles required for EUV applications (~1°-4°) have limited groove efficiencies to less than 27%. Atomic force microscopy (AFM) showed the reason to be rounding of the ideal blaze (sawtooth) groove profile during ion-etching, when a high groove density was combined with the desired low blaze angle. A process developed at Zeiss²⁸ corrects this effect significantly. An ion-etched grating with a relatively high blaze angle (~6°-10°) is immersed in a liquid polymer, withdrawn parallel to the grooves, and then baked. The liquid in the grooves assumes a shape, which modifies the blaze angle to a degree dependent on the liquid and the withdrawal rate. We are engaged in NASA-supported work to optimize the characteristics of test-gratings made using this process and to measure their EUV efficiency after application of multilayers. The gratings have a density of 3600 grooves mm⁻¹ and blaze angles between 2° and 4°. Theoretical models produced using AFM-measured groove profiles from these test-gratings yield groove efficiencies approaching 66%, 50%, and 30% in the first, second, and third orders, respectively. Further studies to improve the groove profile are under way at Zeiss, and will be completed in 2003.

From these results it is clear that multilayer-grating technology has reached a mature state, and predictions of effective area can be regarded as reasonably accurate. Using a MS-EXCEL spreadsheet we calculated the effective area of each *APEX* spectrometer as the simple product of the 6 factors discussed above, thus invoking the scalar assumption. For a few test cases we verified the validity of this assumption using the software package PC Grate 2000 MLX, which is one of the latest in a series of grating modeling programs available from International Intellectual Group (IIG), Inc. This program uses a modified integral method, and we have used earlier versions of it in calculating the efficiency of a bare and coated gratings.^{17,19,20,23} In all tests good agreement was found between the model and the simple product of groove efficiency and multilayer reflectance.

Table 2 shows parameter values for the *APEX* baseline configuration, where each of the 8 color-coded columns corresponds to one of the spectrometers shown in Fig. 3. Black-background row labels identify the spectrometer number and its peak design wavelength. The 8 peak wavelengths were chosen to span the range 90-290 Å somewhat uniformly and to be located near strong lines of astrophysical interest.¹ In the science context (section 1), the shortest two wavebands are most important for CVs and extragalactic studies, the middle four wavebands for stellar coronae studies (designed for the highest resolution), and the longest two or three wavebands for WD studies. Of course, all wavebands are pertinent to ISM studies. White- and tan-background row labels indicate input quantities, while pink- and gray-background row labels are derived quantities.

The uppermost section of rows gives basic grating properties such as radius, groove density, and order. To maximize efficiency all spectrometer orders are positive (inside) so that the diffraction angle () is zero (diffracted order lies on the grating normal). To simplify instrument mechanical design we have varied the grating groove density between spectrometers as the peak wavelength and order vary so that the angle of incidence () and consequently the resolving power are held constant at one of two values (=4.13° or 5.45°; R=8640 or 11400). Multilayer reflectance for each waveband was calculated over a wide range in wavelength. However, practical limitations on MCP detector size truncate this range, and wavelength

limits are indicated in the middle rows of Table 2. We have assumed an active detector size of 50 mm in the dispersion direction, which is a comfortable value with present MCPs. (In practice spacecraft motion will require a slightly large size.)

Table 2. Baseline APEX configuration: Balance Wavelength Coverage and Peak Effective Area

Spectrometer	1	2	3	4	5	6	7	8
Grating Radius (mm)	3000	3000	3000	3000	3000	3000	3000	3000
Detector+Grating Resolution (microns)	25	25	25	25	25	25	25	25
grooves/mm	3600	3000	3600	3170	2715	3600	3200	2940
Order	2	2	2	2	2	1	1	1
angle of incidence (degrees)	4.13	4.13	5.45	5.46	5.45	4.13	4.13	4.13
Resolving Power	8640	8640	11405	11412	11403	8640	8640	8644
Peak Wavelength (Angstroms)	100	120	132	150	175	200	225	245
Detector Active Size (mm)	50	50	50	50	50	50	50	50
Wavelength Range (Angstroms)	23.1	27.8	23.1	26.3	30.7	46.3	52.1	56.7
Lower Limit (Angstroms)	88.4	106.1	120.4	136.9	159.7	176.9	199.0	216.7
Upper Limit (Angstroms)	111.6	133.9	143.6	163.1	190.3	223.1	251.0	273.3
# periods Multilayer (nodal/spacer)	19 B/Rh	12 Be/Mo4Ru6	12 Mo2C/Si	10 Mo2C/Si	6 Mo2C/Si	9 Mo2C/Si	8 Mo2C/Si	7 Mo2C/Si
%Saturation	48.1	48.1	53.4	58.1	50.7	79.2	81.9	81.7
Multilayer Peak Reflectance	0.307	0.361	0.388	0.382	0.287	0.383	0.341	0.308
T _{spacer} (Angstroms)	25.26	30.35	35.10	41.75	50.97	67.93	81.51	91.29
T _{nodal} (Angstroms)	26.61	31.87	33.40	37.16	42.92	38.57	39.10	40.46
Detector Quantum Efficiency	0.55	0.50	0.45	0.42	0.40	0.30	0.30	0.30
Filter Transmission	0.85	0.78	0.74	0.68	0.55	0.50	0.44	0.40
Groove Efficiency	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
Collimator Transmission	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Grating Diameter (cm)	34	34	34	34	34	34	34	34
Geometrical Area (cm ²)	907.9	907.9	907.9	907.9	907.9	907.9	907.9	907.9
Integral (Angstroms cm ²)	315.7	541.5	551.3	628.9	592.6	559.7	552.3	554.4
Wavelength Coverage >	10	cm ² =	150.7	Angstroms Σ Integrals (Angstroms cm ²)=				4296.6

We calculated multilayer reflectance profiles using the number of periods, the materials, and the thickness values for the nodal and spacer layers given in Table 2. The ratio of the nodal material thickness to the period thickness (λ) was optimized for the number of periods. The reflectance profiles were calculated using an in-house program, and optical constants were derived from a number of sources in the literature (e.g., ref. 29 and further updates). Cross-calibration of the results of this program with those from other models such as the PC Grate program and the online software at the Center for X-ray Optics website produces excellent agreement.

A simple two-material design was assumed for all wavebands. In practice some diffusion of materials occurs, and this coupled with finite interface roughness reduces reflectance profiles by a small amount, typically a factor of ~ 0.9 at 100-300 Å. For example, a diffusion layer of Mo_xSi_y can be as thick as 15 Å, a significant fraction of the period, especially at shorter wavelengths. The effects of interface roughness are smaller because multilayers tend to propagate the substrate roughness, and ion-etched gratings have roughness in the range 3-5 Å rms. However, more complex multilayer designs can mitigate the effects of both diffusion and roughness,²³ and thus the two-material designs presented here are reasonable estimates. With increasing number of periods deposited, the multilayer bandpass will narrow, but the peak reflectance will grow until it reaches some "saturation" value, at which point the incident radiation no longer reaches the underlying substrate. The integral coverage attains a shallow peak at some number of periods in between 1 period and the number at saturation. For the APEX baseline configuration, we have chosen to balance peak effective area against wavelength coverage, and therefore the number of periods used is at or near this shallow maximum in integral coverage. The peak reflectance produced by the calculation is shown in Table 2 as well as its ratio to the saturation peak reflectance (%Saturation). We have chosen $\text{Mo}_2\text{C}/\text{Si}$ for the 6 spectrometers with peak wavelengths longer than the Si L-edge at ~ 124 Å. For shorter wavelengths other materials must be used, and we have chosen B/Rh and Be/ Mo_4Ru_6 for the 100-Å and 120-Å wavebands, respectively. We do not claim that these are the only materials possible or even the best. However, Mo/Si and its variants have been the standard at long wavelengths for many years, and much expertise has been gained, so that fabricated saturated multilayers are produced regularly with reflectances within 95% of theoretical limits. Diffusion and fabrication problems may occur with other materials, especially at the shorter wavelengths. However, the choices made here are based on our current experience.

Table 2 illustrates some general properties of multilayers. First, multilayers function as synthetic Bragg crystals with the period thickness an integral number times half the peak wavelength. Hence the nodal and spacer layer thickness increases

with wavelength. Second, the number of periods required for saturation and consequently our non-saturated choices decreases with increasing wavelength. Third, the optical constants of materials are such that multilayers attain their peak performance at $\sim 100\text{-}130 \text{ \AA}$.

The multilayer reflectance profile dominates the variation in A_{eff} over any spectrometer waveband, and therefore filter transmission, groove efficiency, collimator transmission, detector QE, and of course grating area were held constant in each spectrometer waveband at the value determined for the peak multilayer wavelength (Table 2). The multilayer reflectance profiles were multiplied by these quantities to produce A_{eff} curves for each spectrometer. This approximation, which can be refined later to include wavelength variation in QE and filter transmission, is good enough for our purposes here, namely to obtain general knowledge of the *APEX* A_{eff} and how it varies with parameters.

The bottom rows in Table 2 contain three metrics, which are useful in comparing spectrometer performance of alternate configurations. For each spectrometer we calculate the Integral ($A_{\text{eff}} \times \text{Wavelength}$) over the waveband as limited by detector size. The total Integral sum for all spectrometers is also given in the lower right corner. Finally, we calculate the total wavelength coverage at A_{eff} greater than the cutoff value of 10 cm^2 . This value of 150.7 \AA is about 75% of the range $90\text{-}290 \text{ \AA}$.

Finally, although Table 2 was primarily used for calculating A_{eff} , we also calculated a nominal spectrometer resolving power using the simple equation $R = f \sin(\theta) / \Delta x$, where f is the focal length, θ is the angle of incidence, and Δx is the quadratic sum of the detector resolution and the grating aberrations. We have assumed 25 \mu m for this sum, which is an approximation. A more rigorous analysis involving ray-tracing is discussed in section 6; however, this simple approximation is useful in quickly comparing different *APEX* configurations.

Fig. 4 shows the A_{eff} curves for the *APEX* baseline configuration. The 8 spectrometer wavebands overlap, and the black line gives the composite result. Discontinuities in the black line are caused by the waveband cutoffs produced by the finite detector size, and therefore should cause no concerns for calibration difficulties.

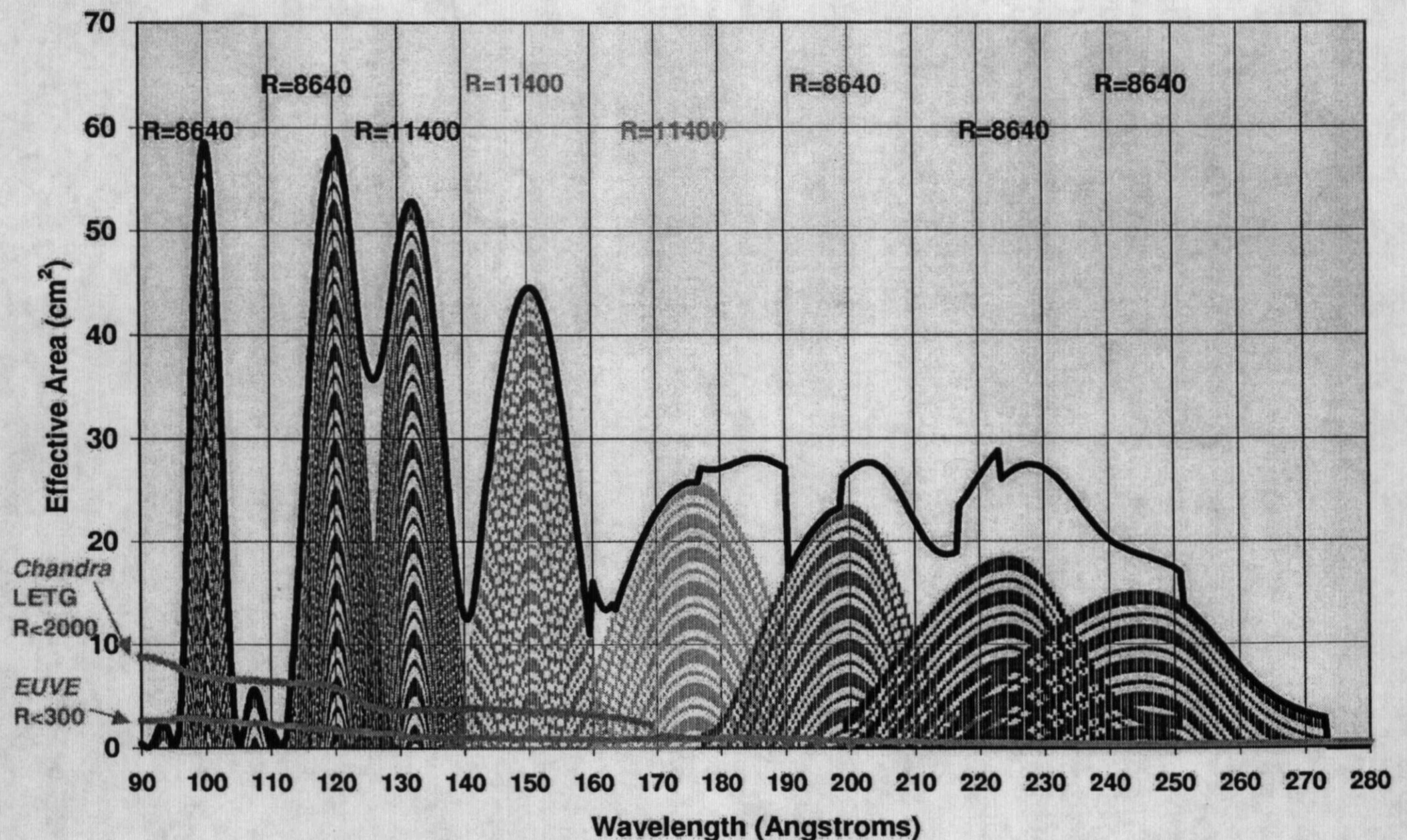


Fig. 4. *APEX* Baseline Configuration: Balance Wavelength Coverage and Peak Effective Area.

Also shown in Fig. 4 is the A_{eff} for the sum of the first orders with the *Chandra* Low Energy Transmission Grating (LETG) as well as the composite A_{eff} for the three *EUVE* spectrometers. *APEX* will achieve peak effective areas of 50-60 cm^2 at selected wavelengths, but with coverage exceeding 10 cm^2 over 75% of the range 90-290 \AA . The peak values exceed the *EUVE* and *Chandra* values by an order of magnitude or more everywhere in the region of overlap, and the *Chandra* LETG response extends only to ~ 170 \AA . More importantly, the *APEX* resolving power exceeds that of *Chandra* by at least a factor of 5, and *EUVE* by a factor of ~ 30 . This combination of simultaneous high effective area and resolving power makes *APEX* an ideal instrument to open a new door in EUV spectroscopy.

5. EFFECTIVE AREA FOR ALTERNATE *APEX* CONFIGURATIONS

We constructed the spreadsheet to investigate quickly how different configurations affect the *APEX* A_{eff} . One of the simplest changes is to deposit enough periods to saturate the multilayers, keeping all other parameters the same as in the baseline case. The results are shown in Fig. 5 and Table 3. The peaks double to ~ 120 cm^2 at 100-120 \AA wavelengths (note the factor of 2 scale change in the ordinate as compared to Fig. 4), but the gain become negligible at longer wavelengths. However, this configuration might be useful if it was decided that monitoring fewer spectral lines with greater sensitivity (perhaps for better temporal resolution) was more desirable than wavelength coverage. Note that the Integral metric for the short wavelength spectrometers increases slightly compared to the results in Table 2, while that for the long wavelength spectrometers decreases in proportion so that the total Integral sum remains approximately constant. It is interesting that the wavelength coverage decreases by only one-sixth to a value of 126.8 \AA .

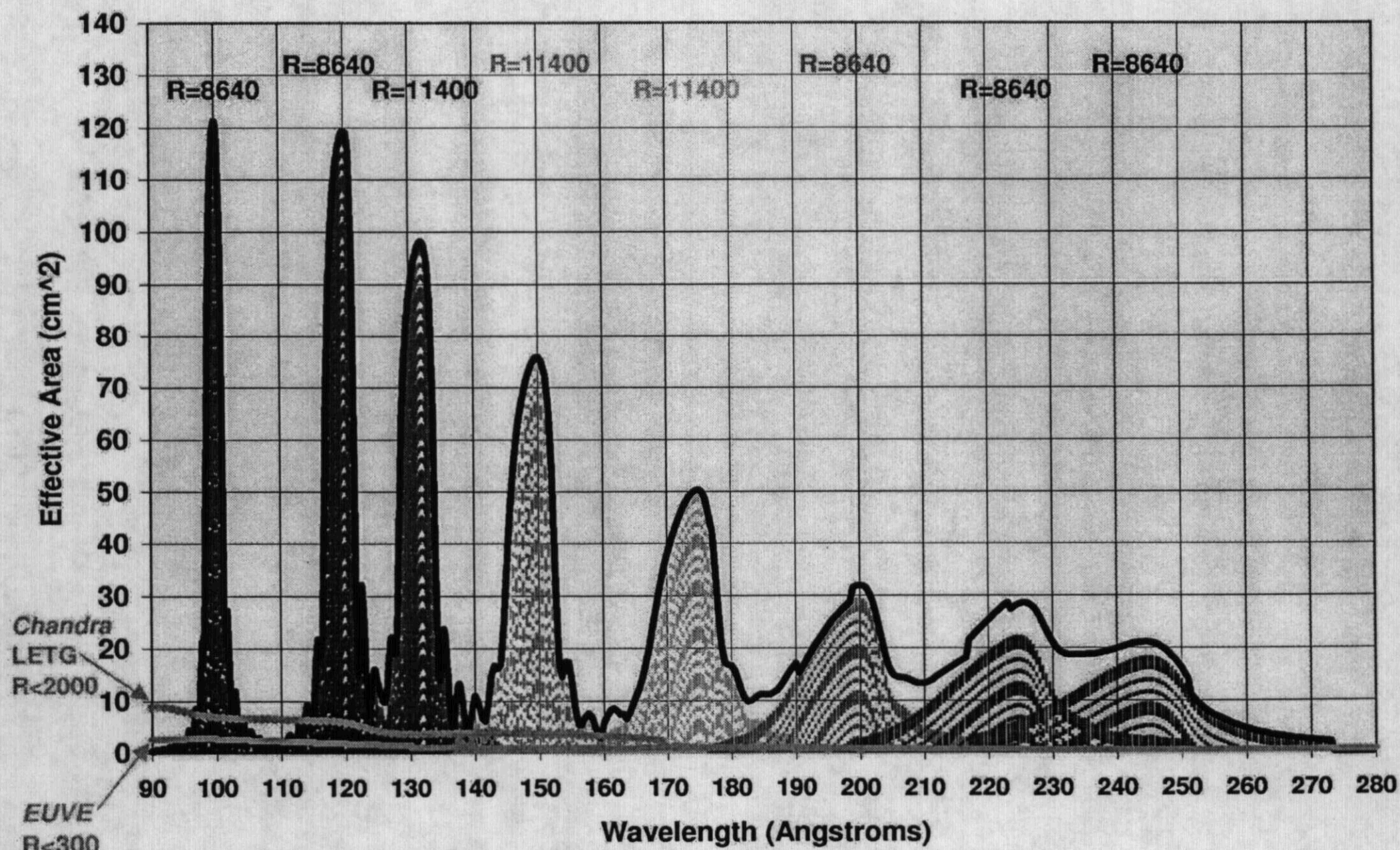


Fig. 5. *APEX* Alternate Configuration: Maximize Peak Effective Area.

Table 3. Alternate *APEX* configuration: Maximize Peak Effective Area

Integral (Angstroms cm^2)	363.5	616.7	605.1	638.9	598.0	491.2	485.1	494.0
Wavelength Coverage >	10	cm^2 =	126.8	Angstroms Σ Integrals (Angstroms cm^2)=				4292.6

Of course hybrid alternates of saturated and non-saturated multilayers are also possible. We examined several other configurations. First, to increase wavelength coverage over 10 cm^2 , we reduced the number of multilayer periods on the 4 shortest wavelength spectrometers so that the summed A_{eff} (black line) was approximately constant at $20\text{-}30 \text{ cm}^2$. However, the gain in wavelength coverage was marginal (154 \AA), making this alternative unappealing. Second we replaced the multilayers with single layers of gold on all spectrometers. A_{eff} dropped to values less than or equal to the *EUVE* values in Figs. 4 and 5 with no coverage over 10 cm^2 , dramatically demonstrating the gain imparted by the multilayer coatings. Third, we varied the detector size between 40 mm and infinity, and we were surprised to discover that strenuous efforts to increase detector size and thereby capture more of the each spectrum were unwarranted. The gain with no detector limit was marginal (153 \AA wavelength coverage above 10 cm^2 and a total Integral sum of 4630 \AA cm^2). In summary, these simple tests showed that even without refining the calculations we could already judge the effects of major design changes on A_{eff} .

However, with a limited number of spectrometers available it is obvious that the biggest arguments will come over placement of wavebands. There is considerable freedom in each selection as it depends solely on multilayer thickness, and small changes can be accommodated easily. In practice the selections would be driven by the scientific objectives as determined by an *APEX* Science Working Group (SWG). Therefore, the SWG can use the spreadsheet as a tool for refining its goals. An objective method might be to weight the scientific value of spectral lines to optimize waveband locations and widths.

One argument that has been raised consistently against EUV instruments is that the transparency of the ISM limits their use to primarily local galactic observations. For at least 2 reasons, this is something of a misperception. First, transparency is a steep function of wavelength. Fig. 6 shows for three different hydrogen densities the distance at which incident radiation is attenuated 90%, as a function of wavelength.³⁰ The galaxy becomes more transparent at wavelengths approaching 100 \AA , and therefore short wavelengths would allow for a broad range of galactic and extragalactic observations. Second the ISM is patchy, and in Fig. 7 we show the accessible space out to 20 pc as a function of wavelength and of galactic coordinates. Coverage is large and although it decreases rapidly for larger distances, holes (e.g., the Lockman hole) provide for a reasonable solid angle for extragalactic work. Finally, *APEX* is not a survey instrument and most likely its targets will be chosen carefully from the present list of EUV sources (~ 1000) provided by the *EUVE* and the *ROSAT WFC* all-sky surveys.

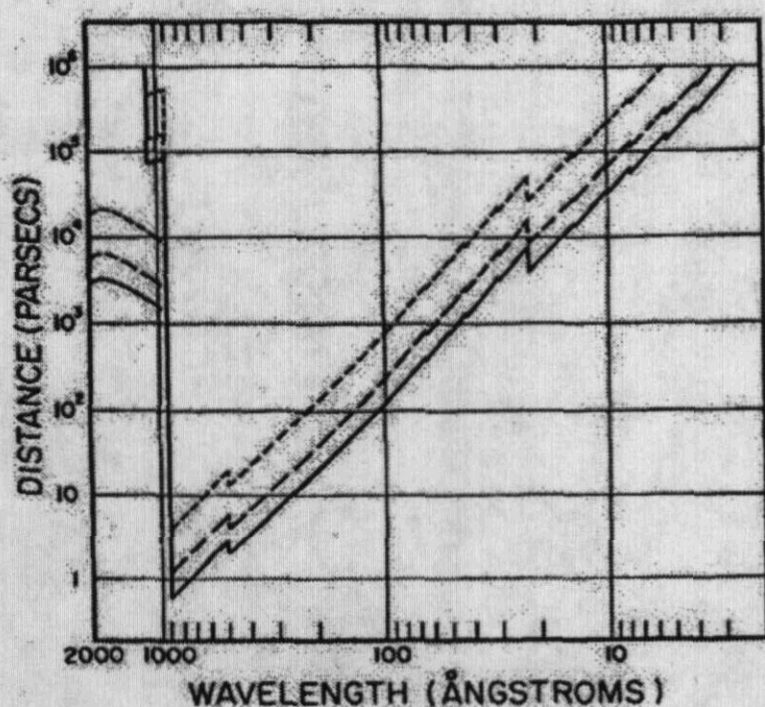


Fig. 6. Distance at which incident radiation is attenuated 90%. An un-ionized ISM of normal composition is assumed with $n_{\text{H}} = 0.2, 0.1$, and 0.03 cm^{-3} , for solid-, long-, and short-dashed curves, respectively.

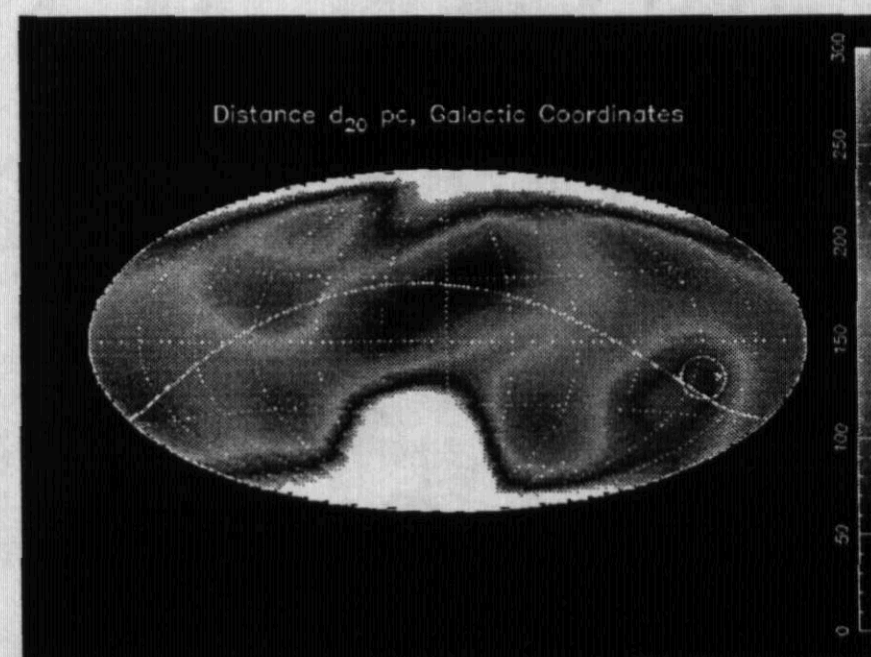


Fig. 7. Accessible space out to 20 pc as a function of galactic coordinates and of wavelength (\AA ; see color legend)

Nevertheless, we have used the *APEX* effective area spreadsheet to construct a radically different configuration that is optimized for wavelengths less than 100 \AA . The results are shown in Fig. 8, where the wavebands are spaced in 5-\AA interval. The configuration balances wavelength coverage with peak effective area for the 6 longest wavebands, but multilayers for the 2 shortest wavelength spectrometers are saturated. Because it has favorable optical constants, a B/Rh multilayer was chosen for these calculations; however, fabrication issues might make other materials such as W/B₄C more practical. The 5 shortest wavelength spectrometers operate in the third grating order, and we have assumed a groove efficiency of 30% to reflect current predictions, resulting in a sharp drop in peak A_{eff} as compared to the longer waveband spectrometers. Although the

peak values of A_{eff} are comparable to those in the *APEX* baseline configuration (Fig. 4), the wavelength coverage greater than 10 cm^2 is only 22.1 \AA , about half of the range. The total Integral sum is only 741.3 \AA cm^2 , about a sixth of the result for the *APEX* baseline configuration. Moreover, the *Chandra* LETG exceeds the peak *APEX* A_{eff} at wavelengths shorter than 70 \AA , although the *APEX* resolution is still better. Thus, any use of wavebands shorter than $\sim 100 \text{ \AA}$ in *APEX* will require judicious choices among science tradeoffs. However, the use of such wavebands in future larger instruments should not be rejected outright, as cosmological objects will large distances will have important spectral lines redshifted to EUV wavebands.

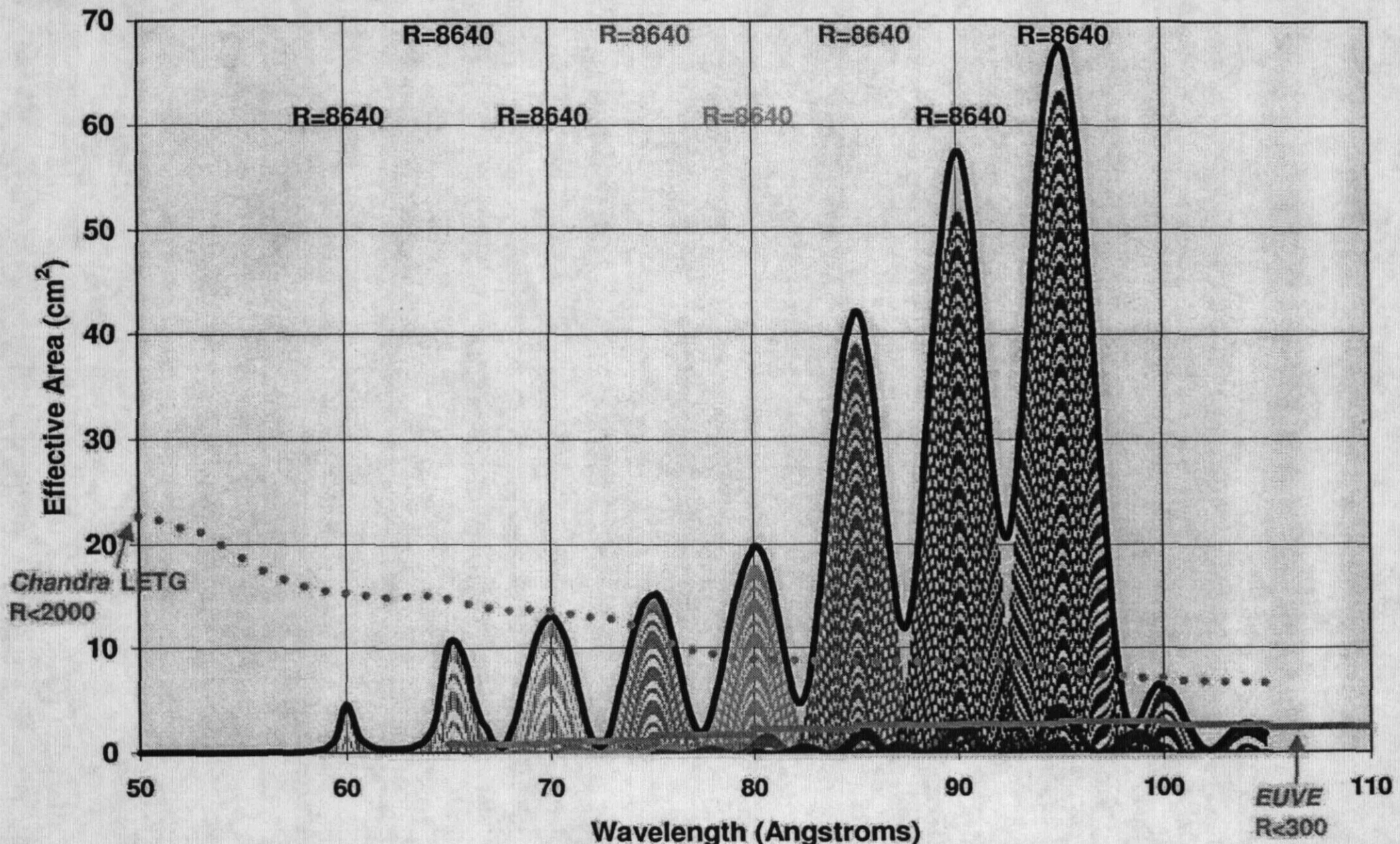


Fig. 8. *APEX* Alternate Configuration: Balance Wavelength and Effective Area at Short Wavelengths

Finally, we calculated A_{eff} curves for a few selected wavebands at wavelengths longer than 300 \AA . Although A_{eff} drops off with increasing wavelength, reasonable observations might be attempted on a number of relatively nearby hot stars with low ISM absorption, for example the giant B stars γ CMa and δ CMa, in which significant understanding can best be accomplished using high-resolution EUV spectra.³¹ Moreover, important and well-known helium transitions occur at 304 \AA and 584 \AA , and abundance measurements of ^3He in the local ISM are cosmologically important.³² With Mo/Si and its variants, the results predict a peak A_{eff} of $\sim 7 \text{ cm}^2$ at 304 \AA decreasing to a peak of $\sim 2 \text{ cm}^2$ at $\sim 500 \text{ \AA}$, compared to $\sim 1 \text{ cm}^2$ for single gold layers. Waveband FWHM increases gradually from 30 to 50 \AA over this range. However, the paucity of targets makes wavebands with peaks longer than 304 \AA unlikely candidates for *APEX*, and such targets will probably have to wait until more suitable instruments can be designed.

6. *APEX* RESOLUTION

The nominal spectrometer resolution given in Figs. 4, 5, and 8 is based on a simple equation derived from focal length and groove density. However, a more rigorous analysis requires ray-tracing. We used the program BEAM FOUR from Stellar Software to create ray-tracing images for the *APEX* baseline configuration spectrometer that peaked at 175 \AA . (Good agreement was found between results from this program and those from in-house software.) Two types of gratings were investigated, the first with a spherical figure and the second with a paraboloidal figure. In both cases, the gratings were mounted in an off-axis Wadsworth mount, with the detector normal going through the center of the grating. Monochromatic ray-tracing images were created at 11 wavelengths separated in 3-\AA intervals over the range $160\text{--}190 \text{ \AA}$. Fig. 9 is a collage of

ray-tracing images located only on the short wavelength side of the multilayer peak, as the images on the long wavelength side were symmetrical. At the multilayer peak wavelength the paraboloidal image has negligible size and is therefore much smaller than the image produced by the spherical grating, which exhibits so-called "spherical aberration" at all wavelengths. However, aberrations for the paraboloidal grating grow faster with off-axis angle and consequently wavelength than for the spherical grating, and the images have a higher degree of asymmetry. At the multilayer's extreme wavelengths as defined for a 50-mm detector (Table 2), paraboloidal and spherical gratings produce images of comparable size

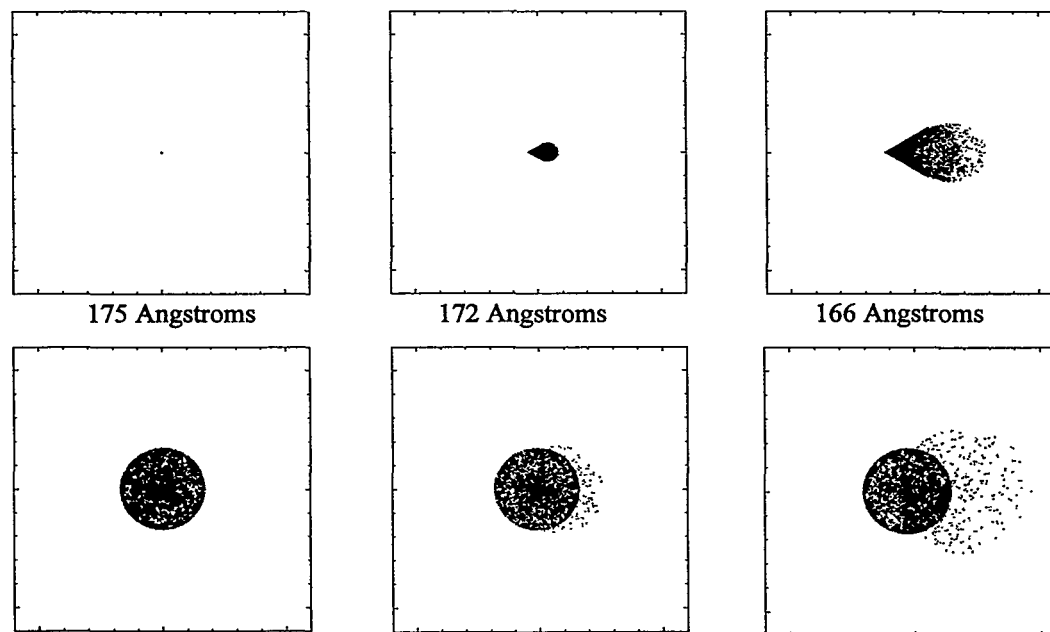


Fig. 9. Ray tracing images at selected wavelengths for a paraboloidal grating (top row) and a spherical grating (bottom row). The image frame size is 120 μ m.

We collapsed the data for each ray-tracing image into a histogram along the dispersion direction (horizontal in Fig. 9), determined the image width at 90% power, and used this value as a measure of grating aberrations. Although images show that grating aberrations are negligible near the multilayer peak wavelength, we conservatively chose a minimum value of 10 μ m for grating aberrations whenever the histogram produced smaller values. These values were added in quadrature to the assumed detector spatial resolution (15 μ m). The resolution curve for the paraboloidal grating, shown in Fig. 10, achieves values near 16,000 at the peak multilayer wavelengths. It exceeds the curve of the spherical grating everywhere over the waveband and exhibits more variation with wavelength. For about half the waveband near its peak wavelength, the resolving power is greater than the nominal value of 11,400 (Table 2), but less than that at the extreme wavelengths. Thus the nominal resolving power calculated from the simple equation represents a reasonable average. Similar results were obtained from analyses of the 100-Å and 245-Å *APEX* spectrometers. In conclusion, this preliminary exercise demonstrates that a paraboloidal figure is preferable to spherical one, and that the *APEX* resolution goals can be achieved.

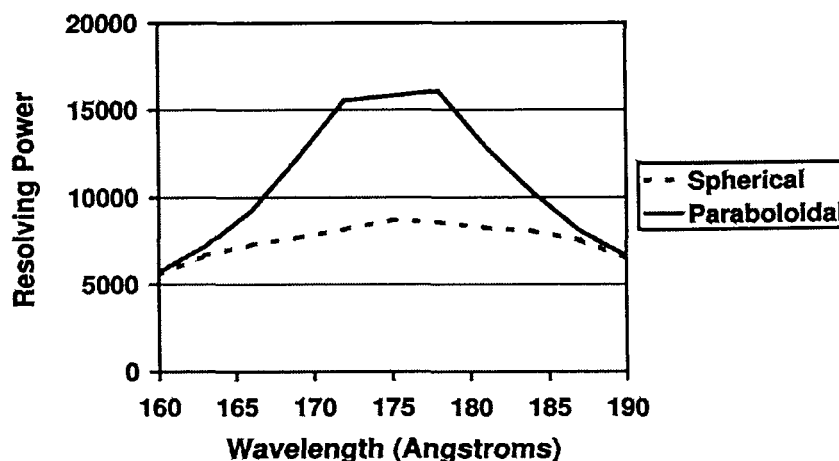


Fig. 10. Resolution curves for paraboloidal and spherical gratings as derived from ray-traced images.

7. CONCLUSIONS

We have presented a practical design for a SMEX satellite instrument, *APEX*, which could be launched by a Taurus booster. *APEX* consists of a suite of 8 spectrometers, each employing a multilayer-coated diffraction grating operating at near-normal incidence and a high-resolution MCP detector. A baseline configuration of *APEX* would achieve peak A_{eff} of 30-60 cm² at selected wavelengths in the range 90-290 Å, with 75% of this range having A_{eff} greater than 10 cm². The average resolving power would be 8640-11400. Variations on the baseline design are also possible, which allow for optimizing the design for a given set of spectral features and for extending or shifting coverage to shorter and/or longer wavelengths. *APEX* would be capable of a wide range of science, particularly in studies of stellar coronae and flares, evolution of WDs, accretion regions in CVs and AGNs, and the nature of the ISM. However, the exact mix of science objectives has yet to be determined. Nevertheless it is clear that high-resolution astronomical spectroscopy, which allows the identification of weak emission lines, the measurement of Doppler shifts and line profiles, and the detection of narrow absorption features, leads to a complete understanding of the density, temperature, abundance, magnetic, and dynamic structure of astrophysical plasmas. Observations at EUV wavelengths are critical to understanding plasmas with temperatures in the range 10⁵-10⁸ K.

The technological and theoretical experience in high-reflectance multilayers and ultrasmooth diffraction gratings of accurate groove profile has been developed in over a decade of research so that efficiencies approaching theoretical limits are now being obtained. This maturity provides *APEX* with a wide design margin, with little technical and consequently programmatic risk involved.

8. ACKNOWLEDGEMENTS

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